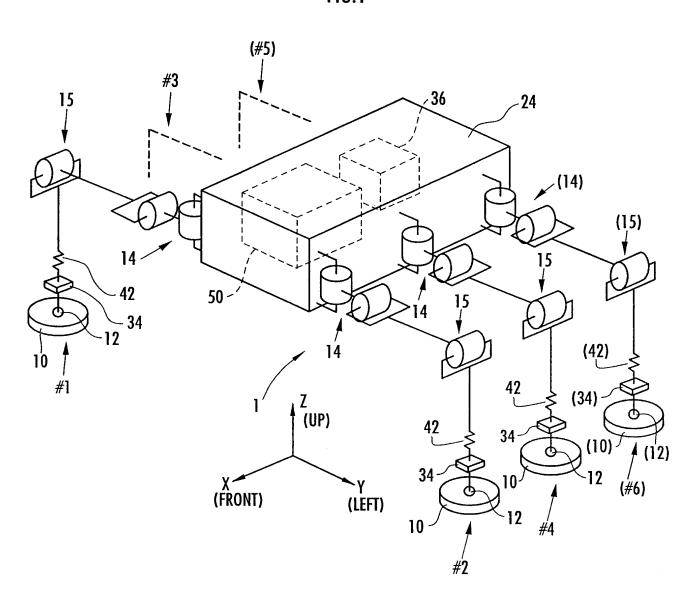
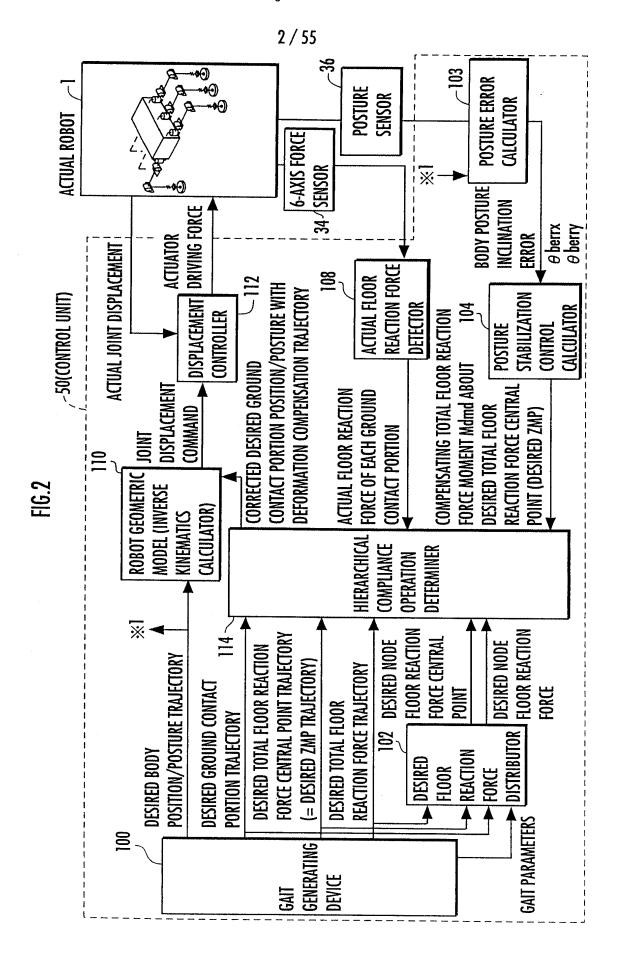
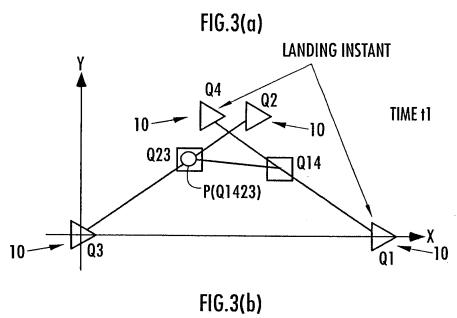
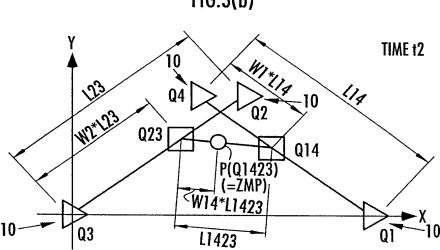
FIG.1

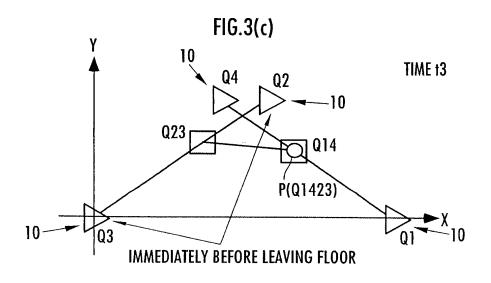




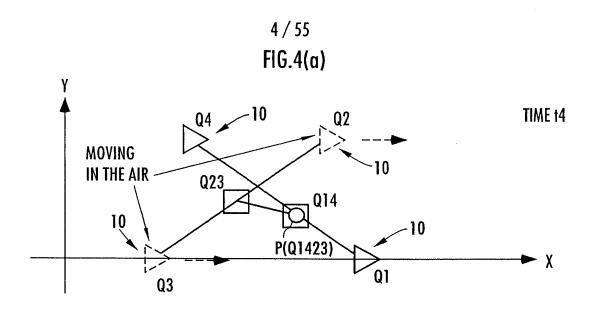
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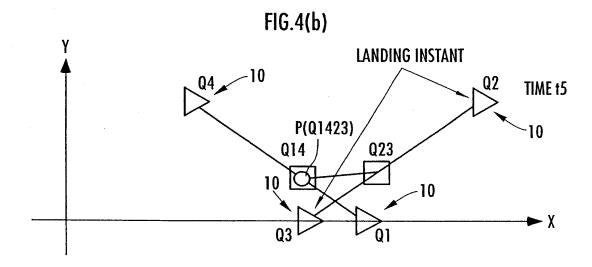


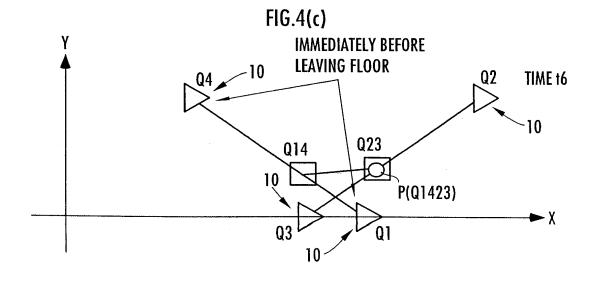


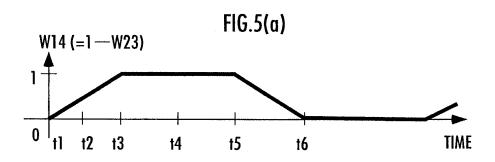


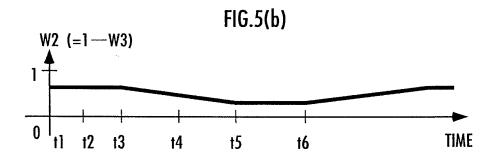
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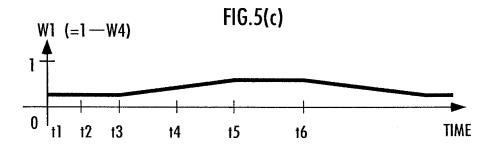


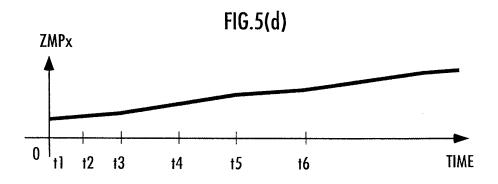




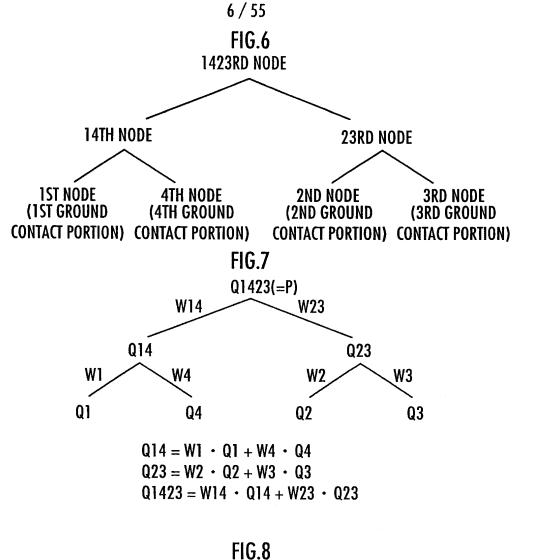


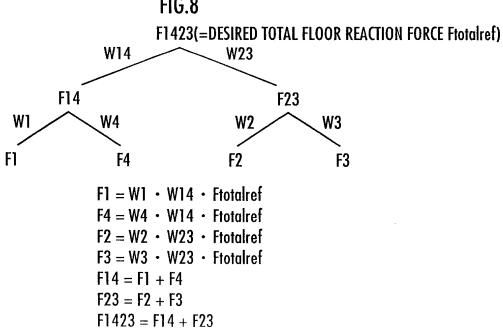




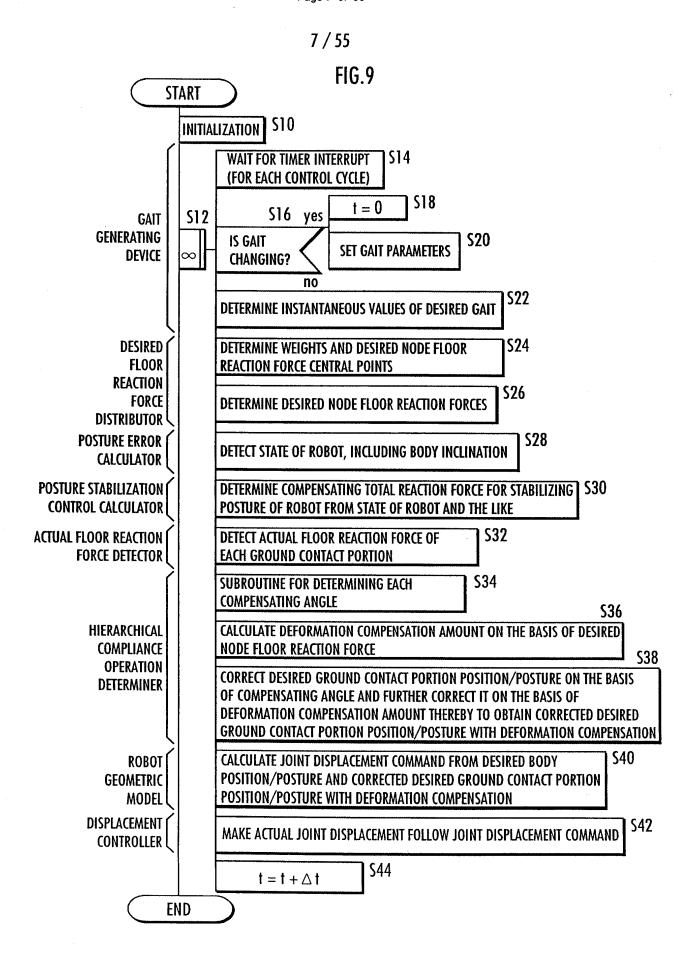


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FIG.10

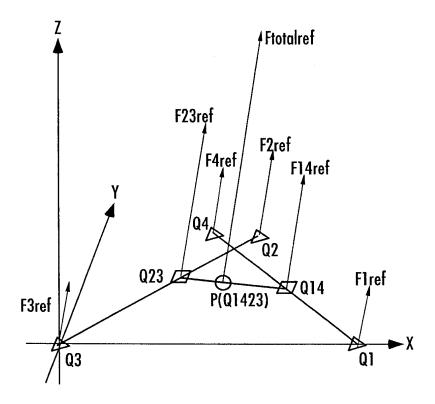
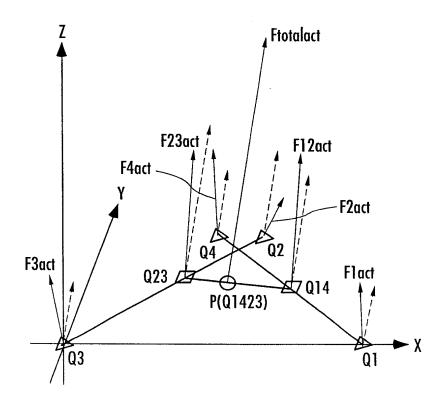
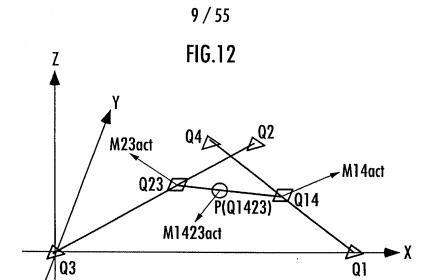
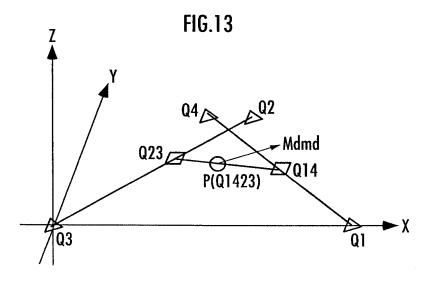


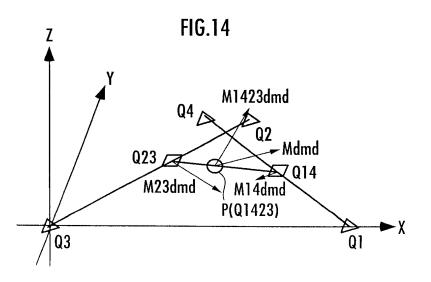
FIG.11



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FIG.15

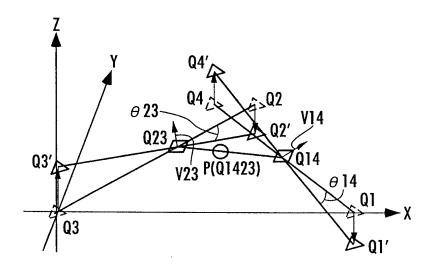
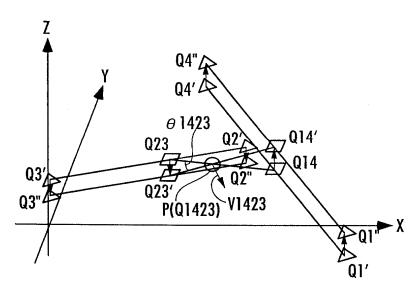


FIG.16



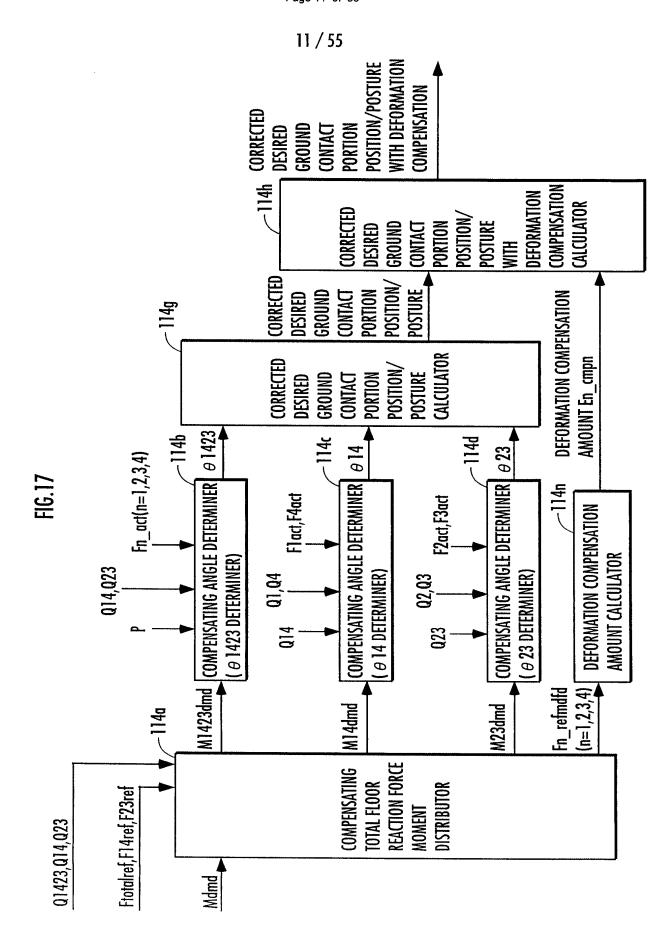
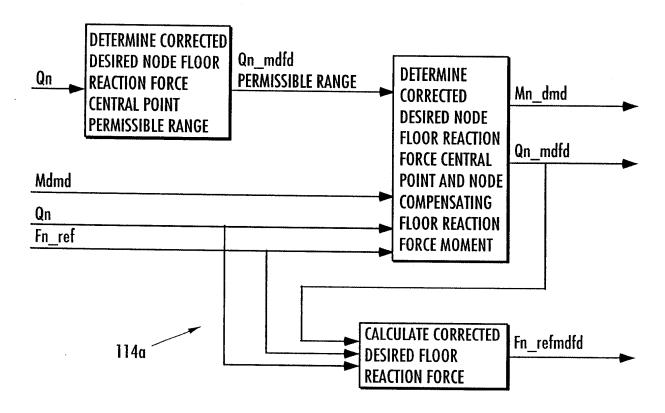
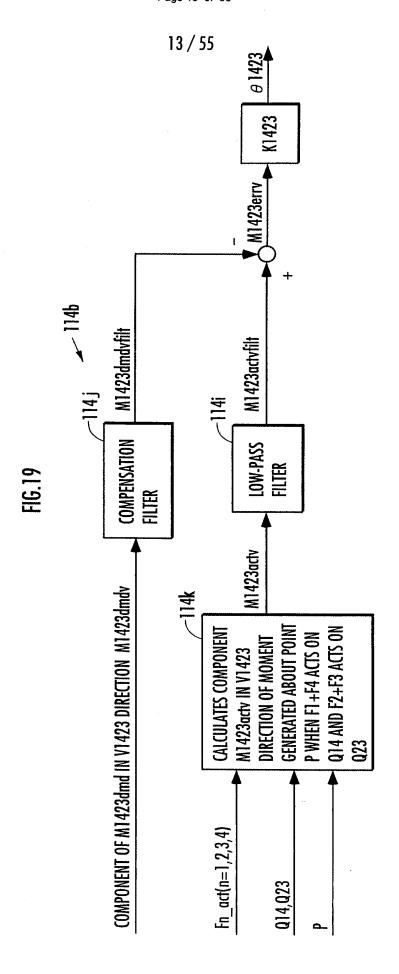
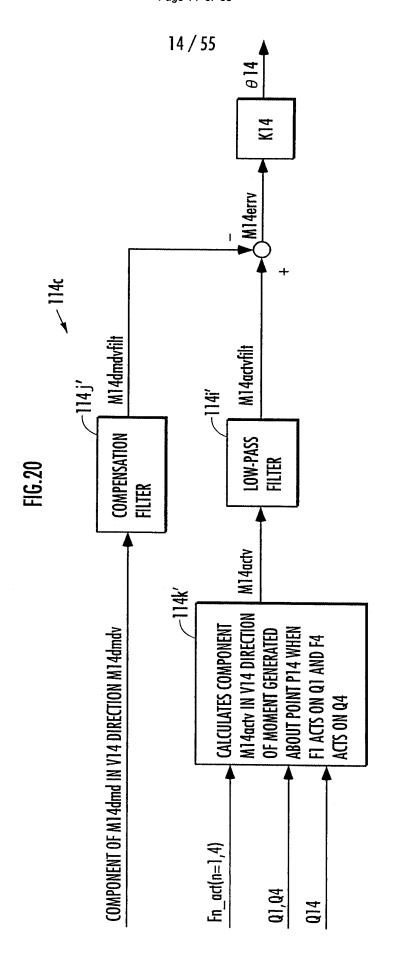


FIG.18

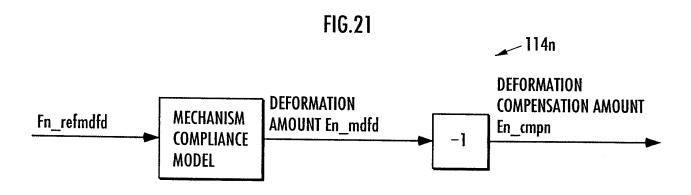




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FIG.22

ENTRY

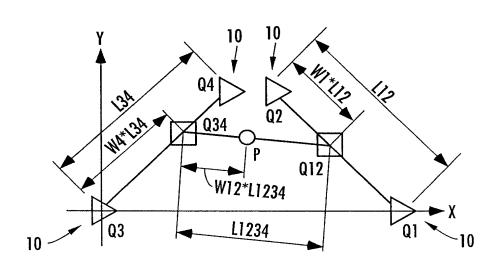
S100 CALCULATE ACTUAL n-TH NODE FLOOR REACTION FORCE Fn_act(n=1,2,3,4,14,23,1423) ON THE BASIS OF ACTUAL FLOOR REACTION FORCE OF EACH GROUND CONTACT PORTION **S102** CALCULATE ACTUAL n-TH NODE FLOOR REACTION FORCE MOMENT Mn_act(n=1,2,3,4,14,23,1423) **S104** DETERMINE n-TH NODE COMPENSATING FLOOR REACTION FORCE MOMENT Mn_dmd(n=14,23,1423) ON THE BASIS OF COMPENSATING TOTAL FLOOR REACTION FORCE MOMENT **S106** DETERMINE VECTORS V1423,V14,V23 AND VECTORS U1423,U14,U23 ORTHOGONAL THERETO, AS DEFINED IN HIERARCHICAL COMPLIANCE OPERATION **S108** EXTRACT COMPONENT IN Vn DIRECTION Mn actv AND COMPONENT IN Un DIRECTION Mn_actu OF ACTUAL n-TH NODE FLOOR REACTION FORCE MOMENT (n=14,23,1423) **S110** EXTRACT COMPONENT IN Vn DIRECTION Mn dmdv AND COMPONENT IN Un DIRECTION Mn_dmdu OF n-TH NODE COMPENSATING FLOOR REACTION FORCE MOMENT Mn dmd(n=14,23,1423) **S112** DETERMINE V COMPONENT OF n-TH NODE COMPENSATING ANGLE BY MULTIPLYING DIFFERENCE BETWEEN VALUE OBTAINED BY PASSING Mn acty THROUGH FILTER AND VALUE OBTAINED BY PASSING Mn dmdv THROUGH FILTER BY GAIN Kn \$114 DETERMINE U COMPONENT OF n-TH NODE COMPENSATING ANGLE BY MULTIPLYING DIFFERENCE BETWEEN VALUE OBTAINED BY PASSING Mn actu THROUGH FILTER AND VALUE OBTAINED BY PASSING Mn dmdu THROUGH FILTER BY GAIN Kn

RETURN

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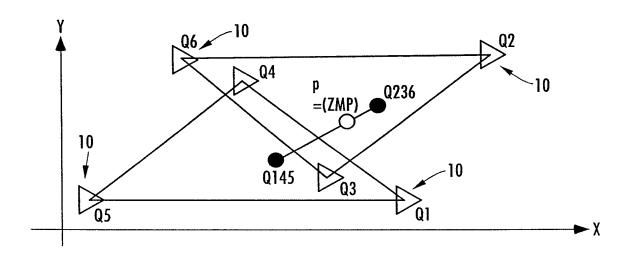
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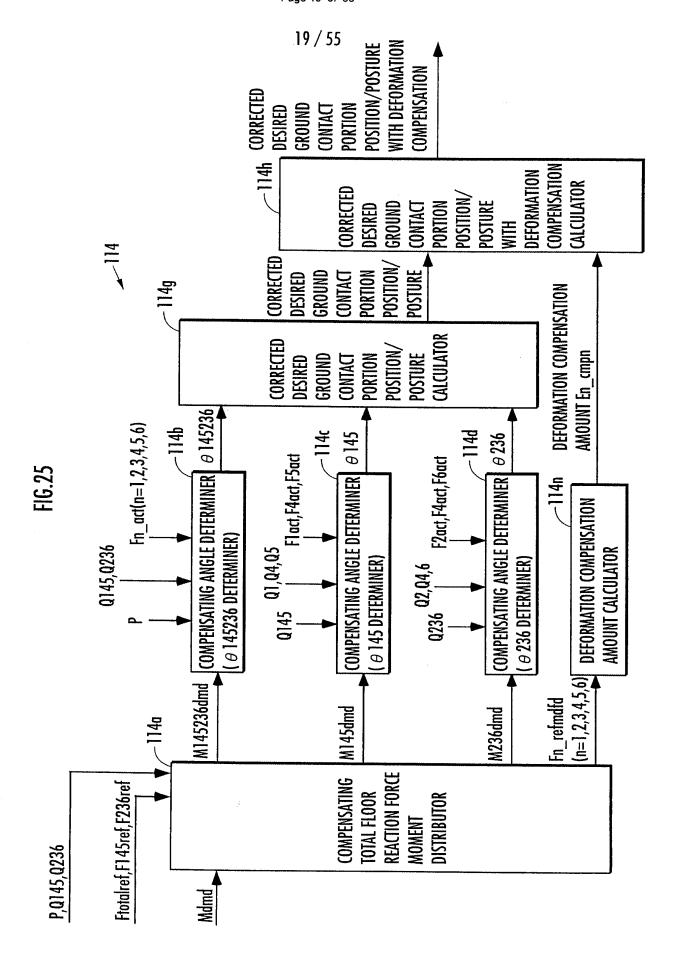
FIG.23



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FIG.24





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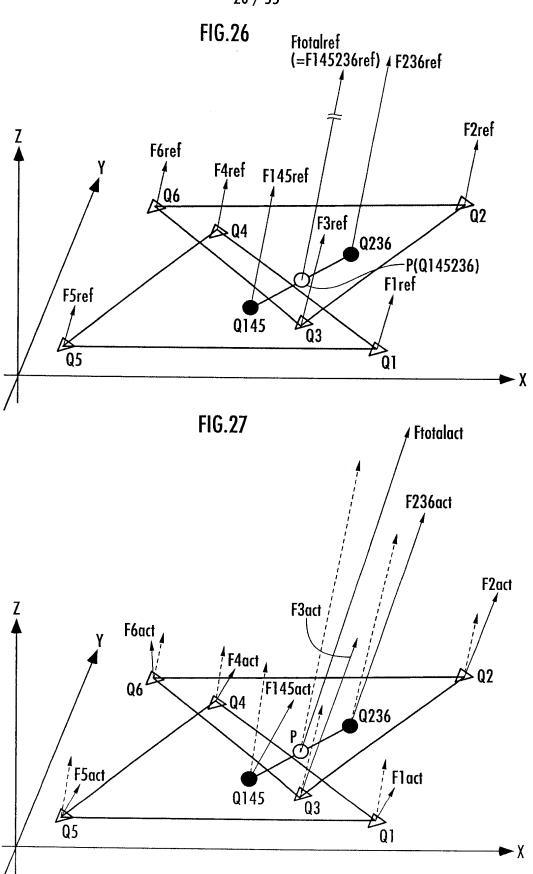
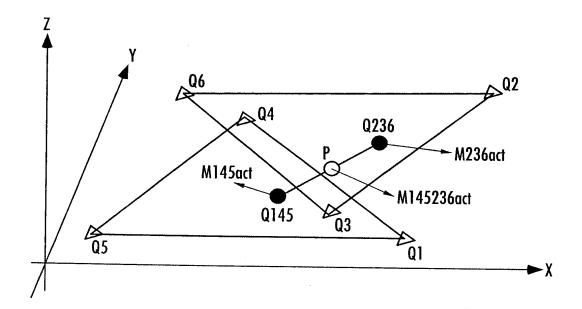


FIG.28



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FIG.29(a)

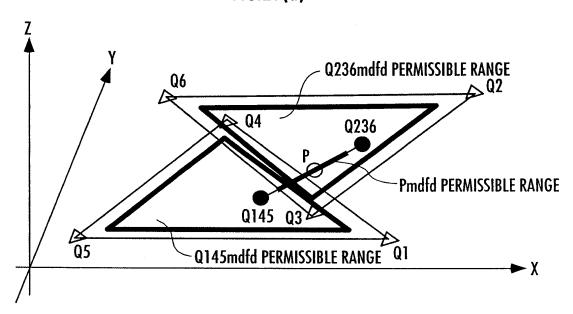
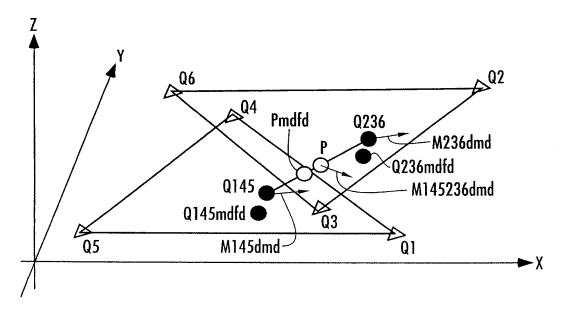


FIG.29(b)



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FIG.30

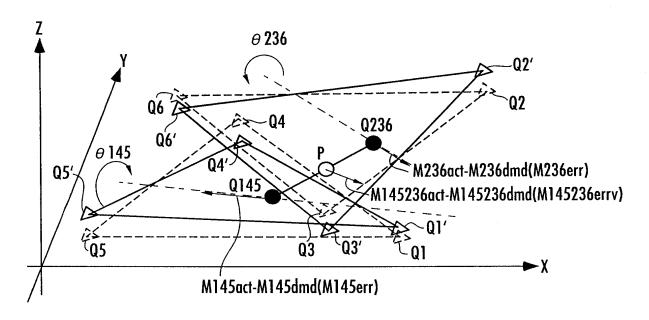
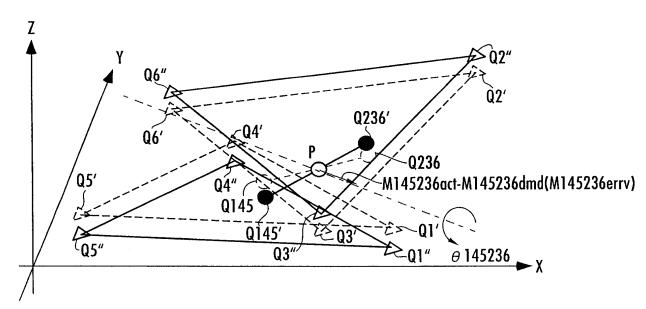
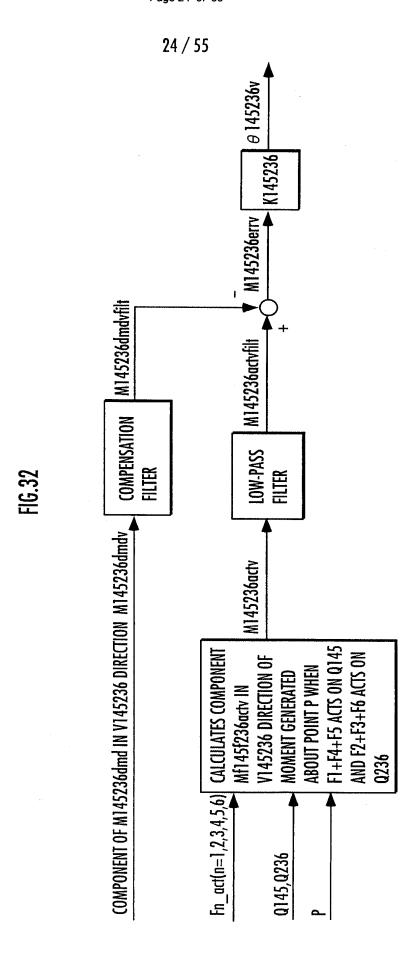
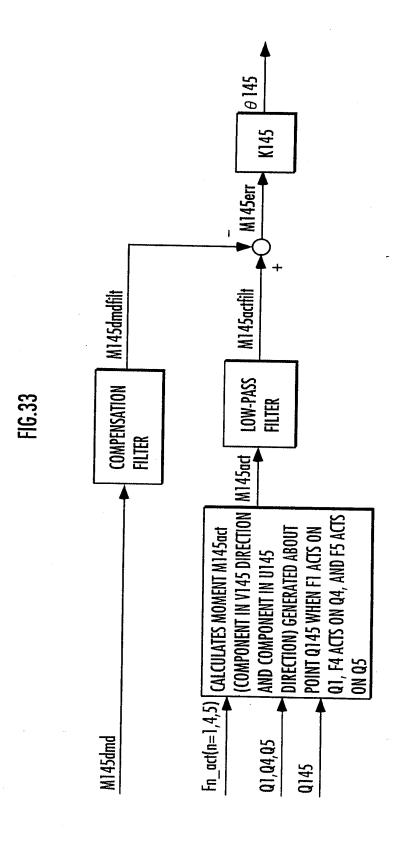


FIG.31



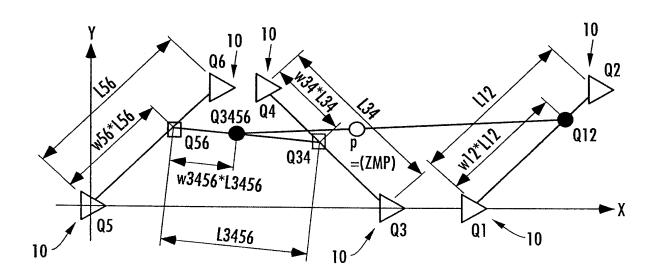


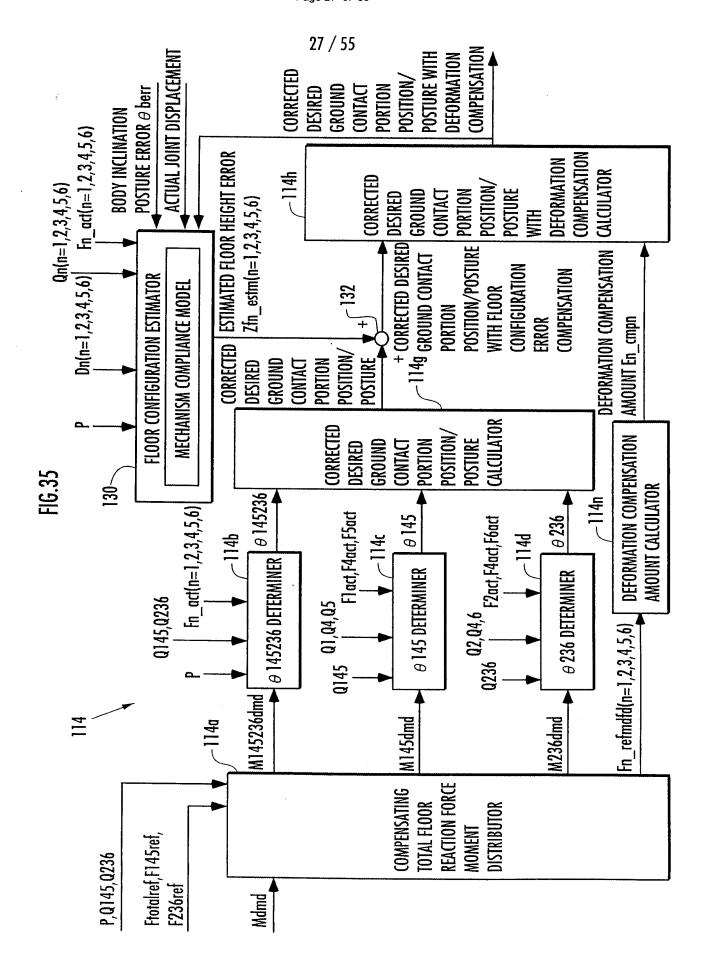
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FIG.34





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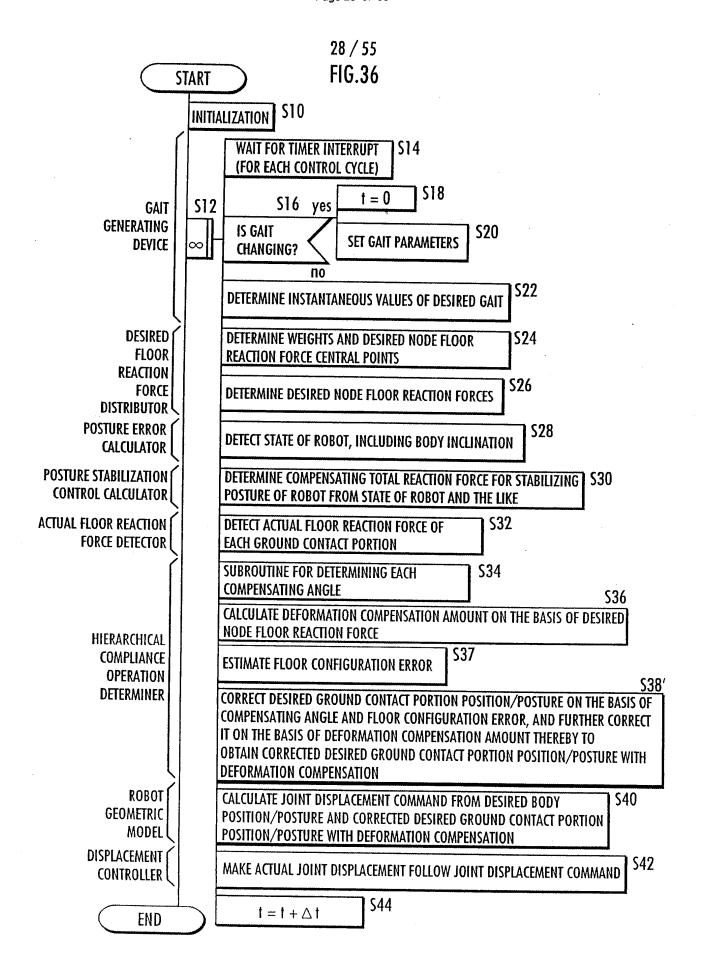


FIG.37

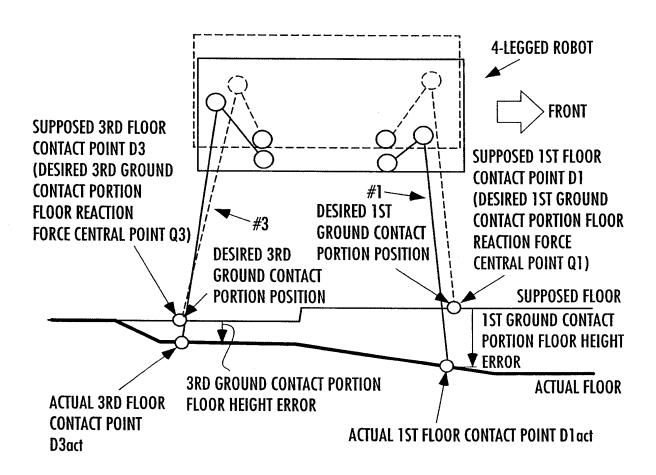
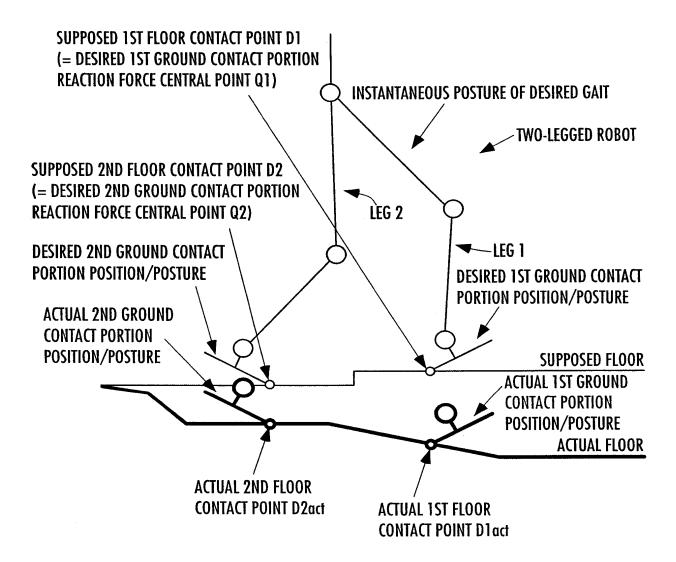


FIG.38





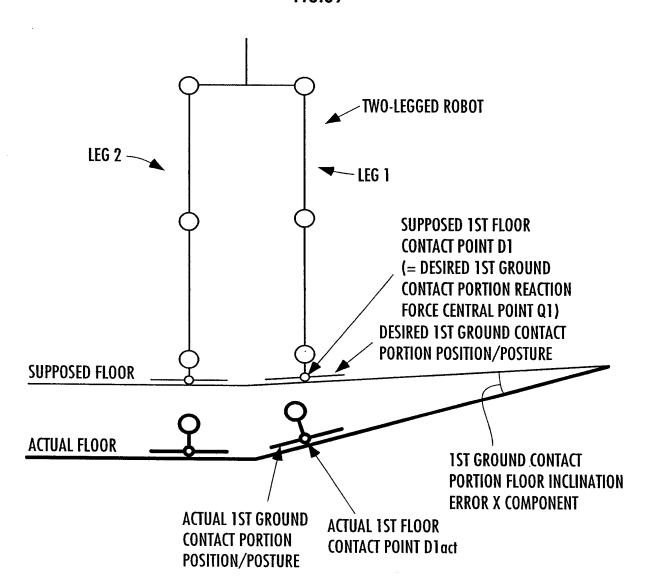


FIG.40

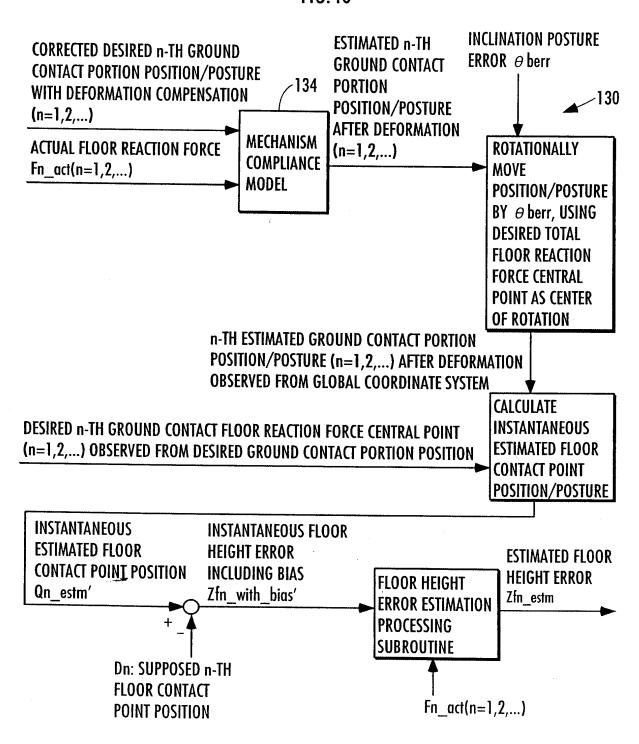


FIG.41

ENTRY

HIERARCHICALLY RELATIVIZE BIAS-INCLUDED INSTANTANEOUS n-TH GROUND CONTACT PORTION FLOOR HEIGHT ERROR Zfn_with_bias' TO DETERMINE INSTANTANEOUS n-TH NODE RELATIVE FLOOR HEIGHT ERROR Zn_rel'

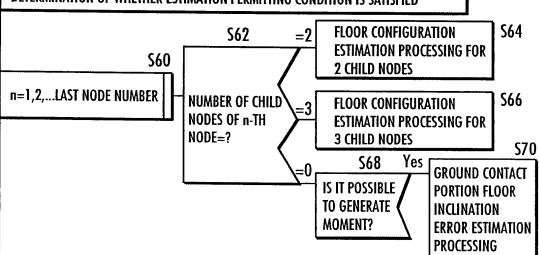
HIERARCHICALLY RELATIVIZE ESTIMATED n-TH GROUND CONTACT PORTION FLOOR HEIGHT ERROR Zfn_estm_p, WHICH HAS BEEN DETERMINED AT LAST CONTROL CYCLE, BY USING CURRENT WEIGHT TO DETERMINE LAST ESTIMATED n-TH NODE RELATIVE FLOOR HEIGHT ERROR Zn_rel_estm_p

 $Zn_{inc_cand} = (Zn_{rel'} - Zn_{rel_estm_p})$ * $\Delta T / (Testm + \Delta T)$

DETERMINE NODE REQUEST MODE OF EACH NODE ON THE BASIS OF TIMING OF DESIRED GAIT

\$56

DETERMINE EACH NODE MODE ON THE BASIS OF NODE REQUEST MODE AND RESULT OF DETERMINATION OF WHETHER ESTIMATION PERMITTING CONDITION IS SATISFIED



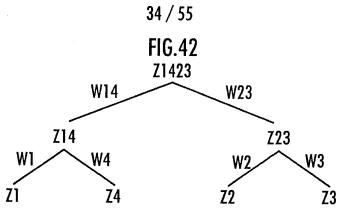
DETERMINE SUM OF ESTIMATED RELATIVE FLOOR HEIGHT ERRORS OF ALL ANCESTOR NODES OF n-TH NODE (n=1,2,...LAST LEAF NODE NUMBER) AND ESTIMATED n-TH NODE RELATIVE FLOOR HEIGHT ERROR, AND DEFINE THE DETERMINED SUM AS ESTIMATED n-TH GROUND CONTACT PORTION FLOOR HEIGHT ERROR Zfn_estm

S72

S52

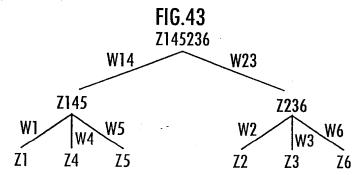
S58

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Z14_with_bias = W1 • Z1_with_bias + W4 • Z4_with_bias
Z23_with_bias = W2 • Z2_with_bias + W3 • Z3_with_bias
Z1423_with_bias = W14 • Z14_with_bias + W23 • Z23_with_bias

Z1_rel = Z1_with_bias - Z14_with_bias
Z4_rel = Z4_with_bias - Z14_with_bias
Z2_rel = Z2_with_bias - Z23_with_bias
Z3_rel = Z3_with_bias - Z23_with_bias
Z14_rel = Z14_with_bias - Z1423_with_bias
Z23_rel = Z23_with_bias - Z1423_with_bias



Z145_with_bias = W1 · Z1_with_bias + W4 · Z4_with_bias + W5 · Z5_with_bias Z236_with_bias = W2 · Z2_with_bias + W3 · Z3_with_bias + W6 · Z6_with_bias Z145236_with_bias = W145 · Z145_with_bias + W236 · Z236_with_bias

Z1_rel = Z1_with_bias - Z145_with_bias
Z4_rel = Z4_with_bias - Z145_with_bias
Z5_rel = Z5_with_bias - Z145_with_bias
Z2_rel = Z2_with_bias - Z236_with_bias
Z3_rel = Z3_with_bias - Z236_with_bias
Z6_rel = Z6_with_bias - Z236_with_bias
Z145_rel = Z145_with_bias - Z145236_with_bias
Z236_rel = Z236_with_bias - Z145236_with_bias

FIG.44

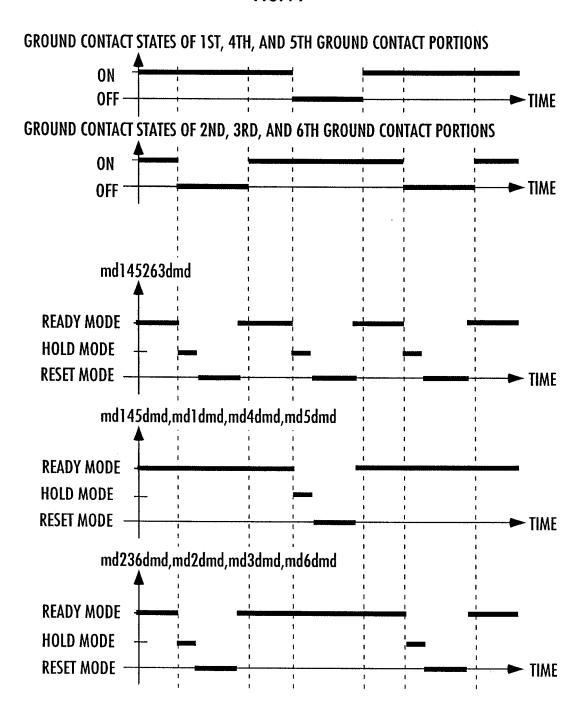
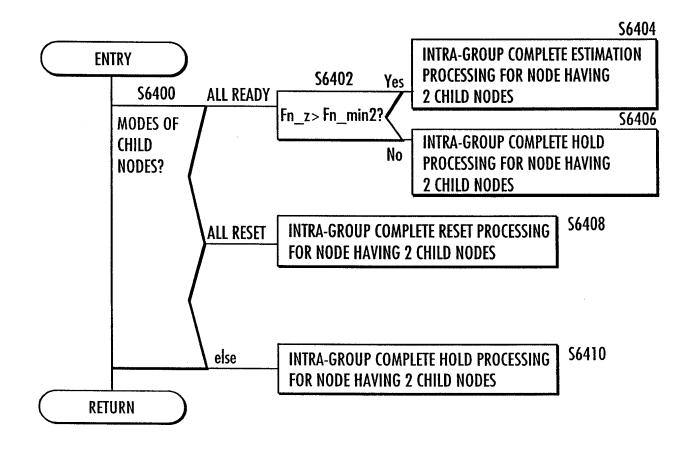
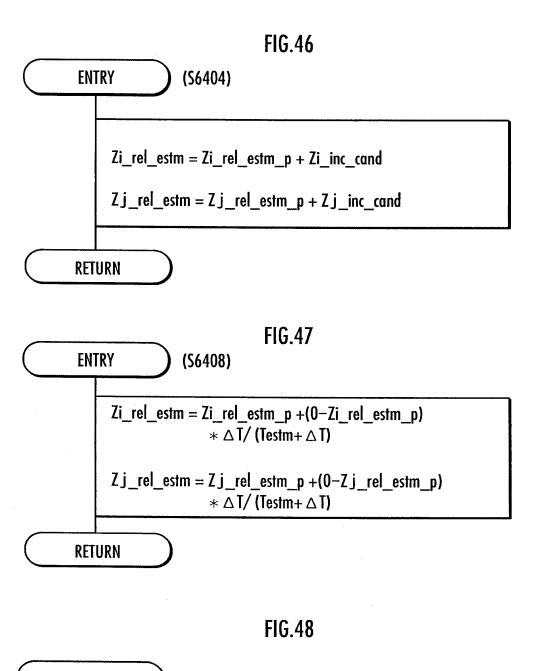


FIG.45

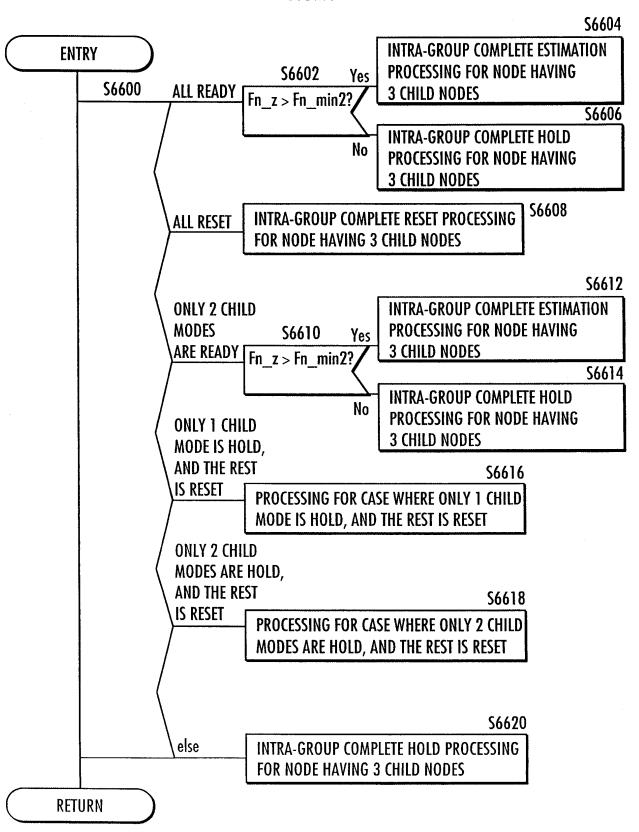




```
| CS6406,S6410)
| Zi_rel_estm = Zi_rel_estm_p
| Zj_rel_estm = Zj_rel_estm_p
| RETURN
```

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FIG.49



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FIG.50

Zi_rel_estm = Zi_rel_estm_p + Zi_inc_cand

Z j_rel_estm = Z j_rel_estm_p + Z j_inc_cand

Zk_rel_estm = Zk_rel_estm_p + Zk_inc_cand

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FIG.51

ENTRY

(\$6608)

$$Zi_rel_estm = Zi_rel_estm_p + (0 - Zi_rel_estm_p)$$

$$* \triangle T/(Testm + \triangle T)$$

$$Z_j_rel_estm = Z_j_rel_estm_p + (0 - Z_j_rel_estm_p)$$

 $* \Delta T/(Testm + \Delta T)$

$$Zk_rel_estm = Zk_rel_estm_p + (0 - Zk_rel_estm_p)$$

$$* \triangle T/(Testm + \triangle T)$$

RETURN

FIG.52

ENTRY

(\$6606,\$6614,\$6620)

RETURN

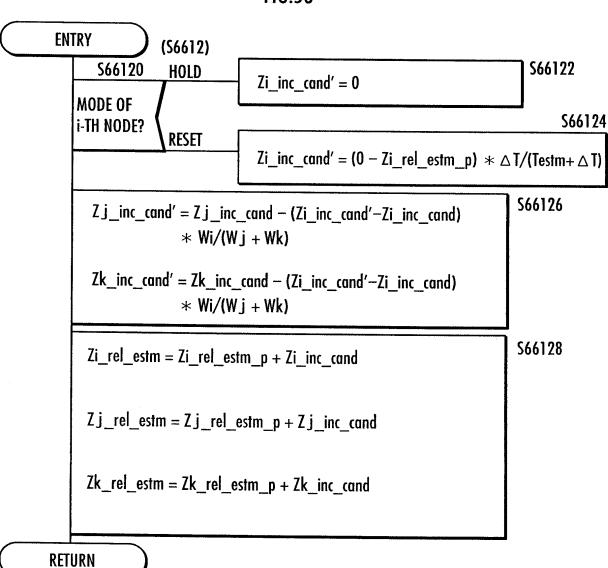


FIG.54

ENTRY

(\$6616)

$$Zi_rel_estm = 0$$

$$Z_j_rel_estm = Z_j_rel_estm_p + (0 - Z_j_rel_estm_p)$$

 $* \triangle T/(Testm + \triangle T)$

$$\begin{tabular}{ll} Zk_rel_estm = Zk_rel_estm_p + (0 - Zk_rel_estm_p) \\ &* \triangle T/(+ \triangle T) \end{tabular}$$

RETURN

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FIG.55

ENTRY

(\$6618)

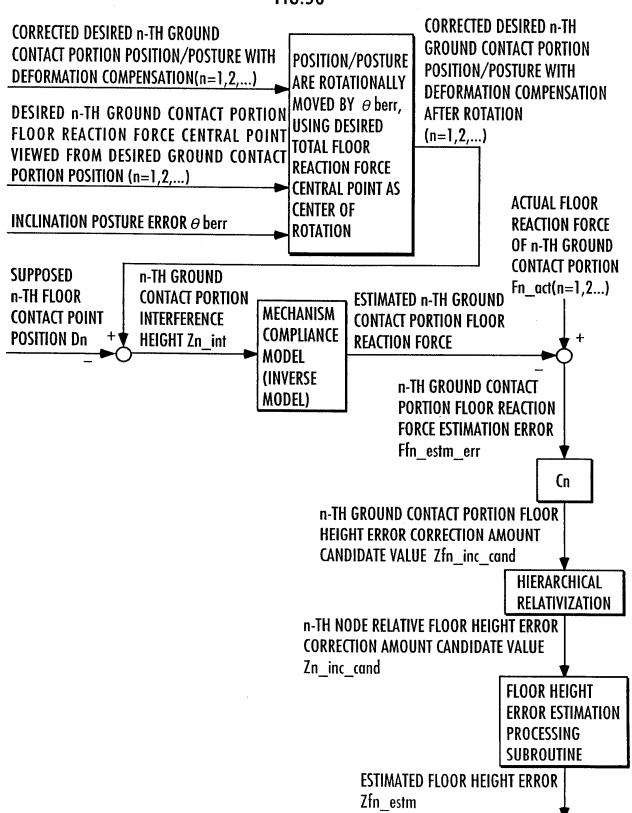
$$Zk_rel_estm = Zk_rel_estm_p + (0 - Zk_rel_estm_p)$$

$$* \triangle T/(Testm + \triangle T)$$

RETURN

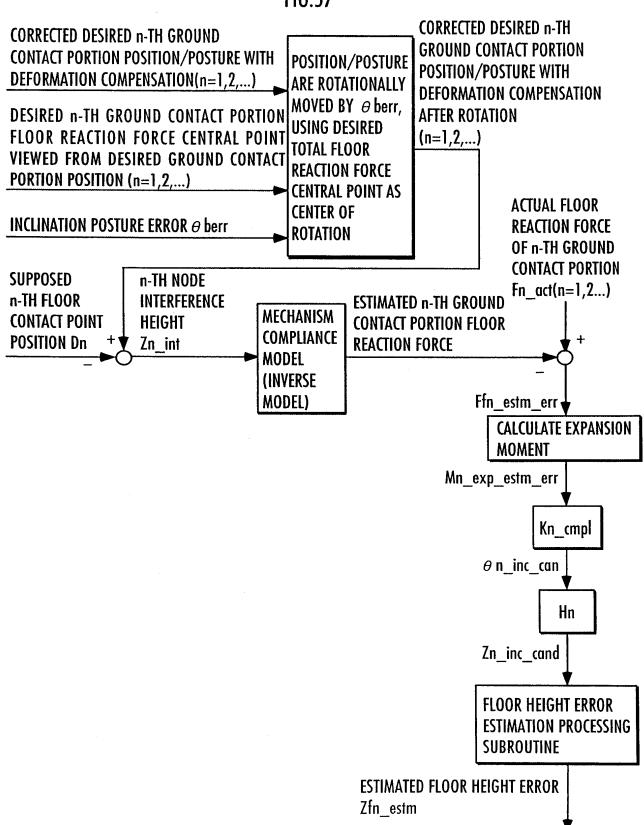
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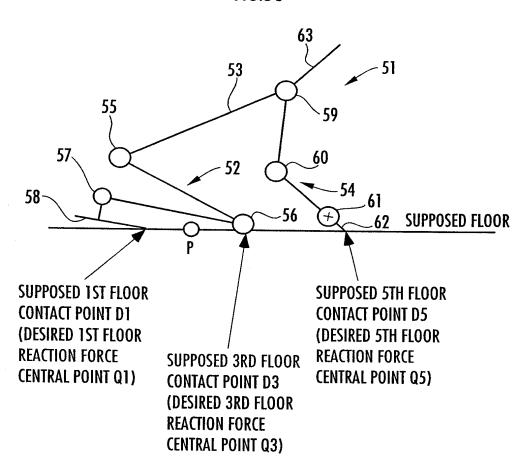
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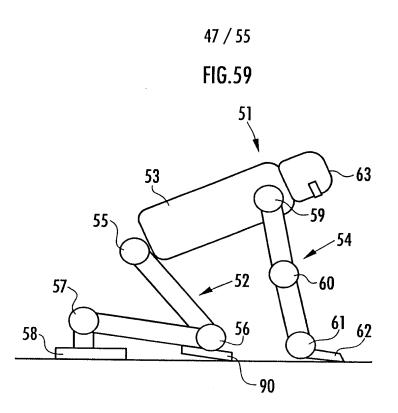
Title: "CONTROL DEVICE FOR MOBILE BODY"
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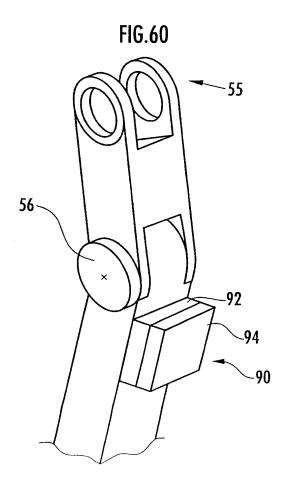
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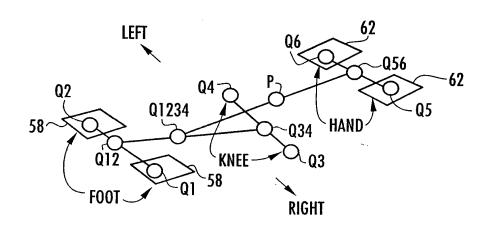
Title: "CONTROL DEVICE FOR MOBILE BODY" First Named Inventor: Toru Takenaka National Stage of PCT/JP2004/018072 Customer No. 40854; Docket No. SAT-16647 Page 47 of 55

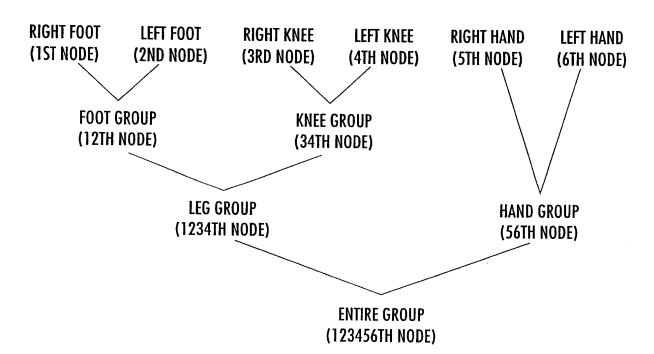


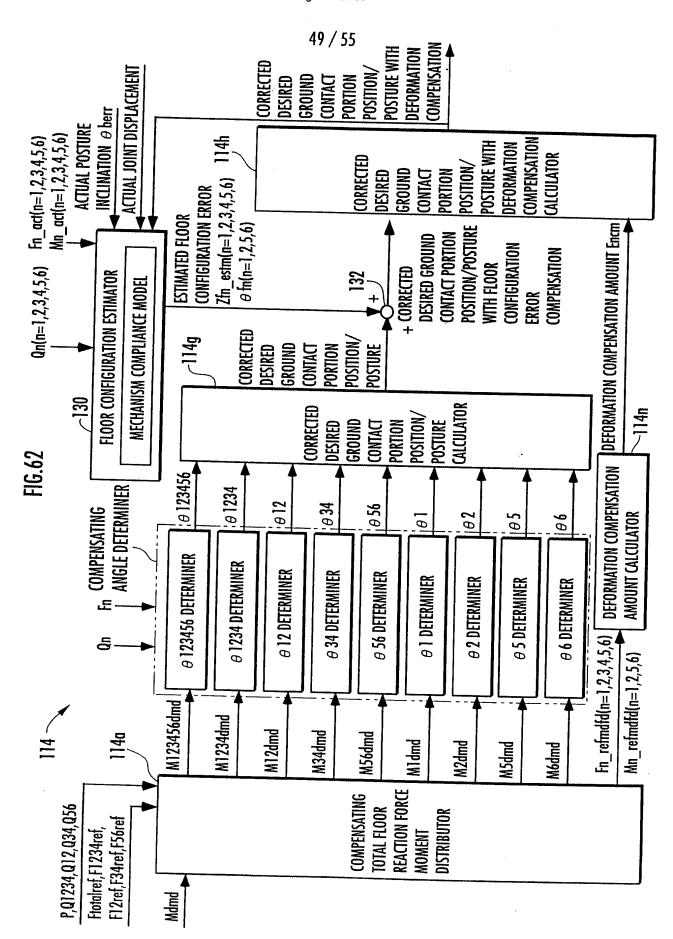


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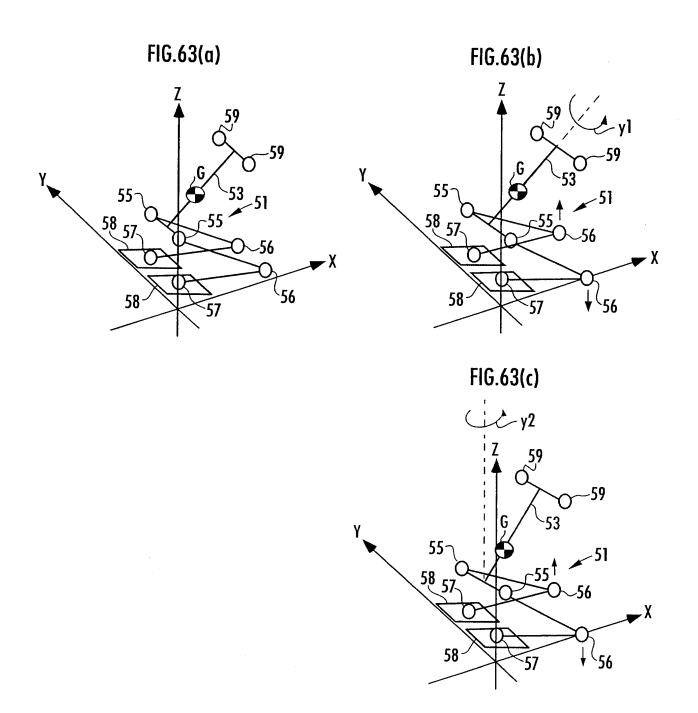
FIG.61





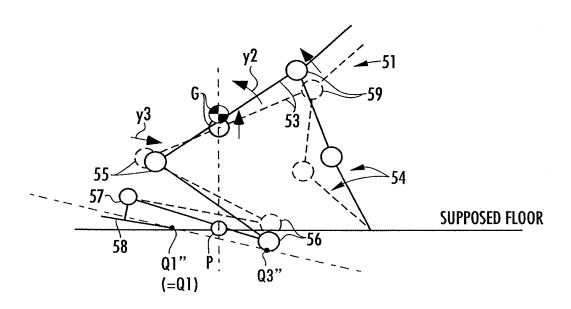


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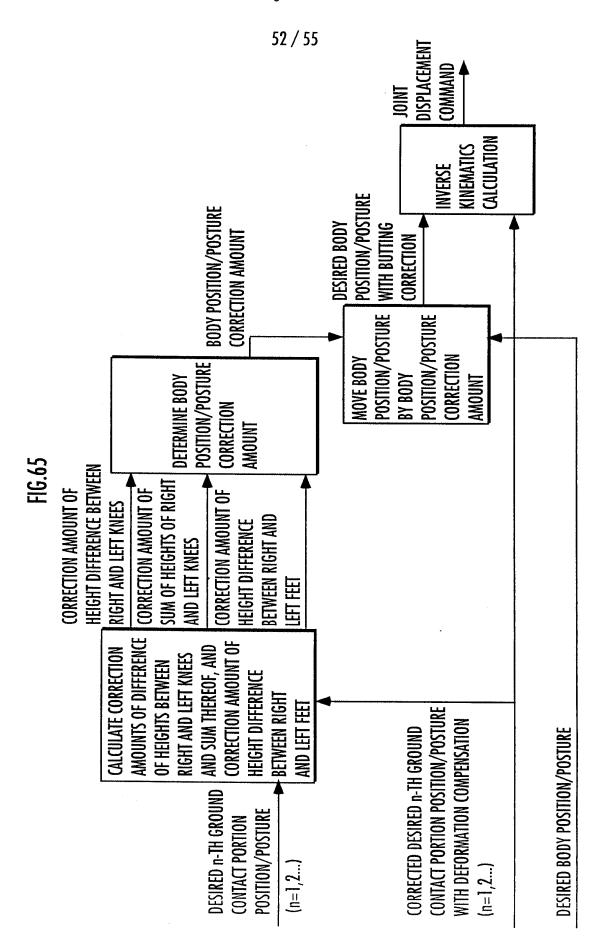


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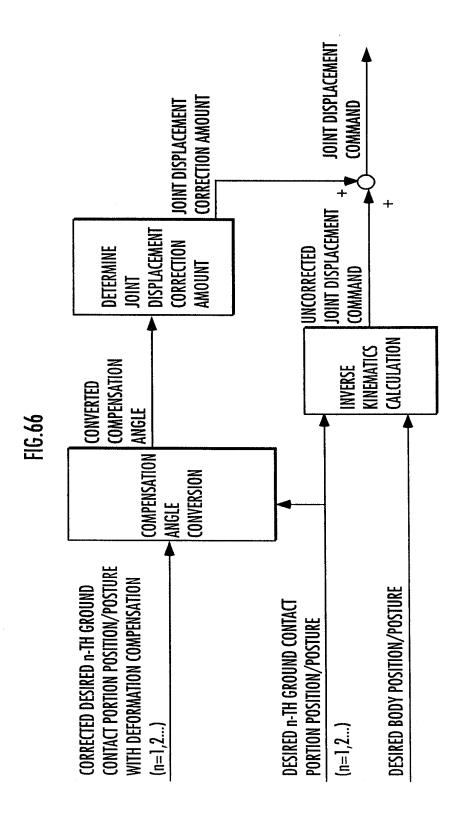
FIG.64



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FIG.67

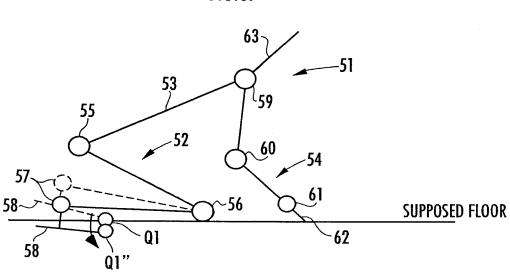
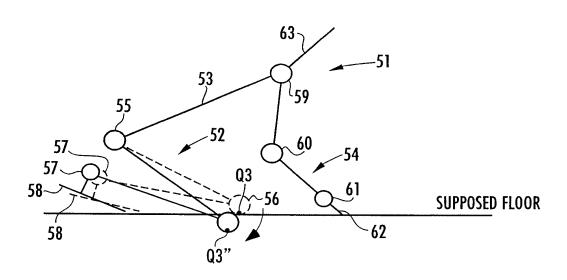


FIG.68



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